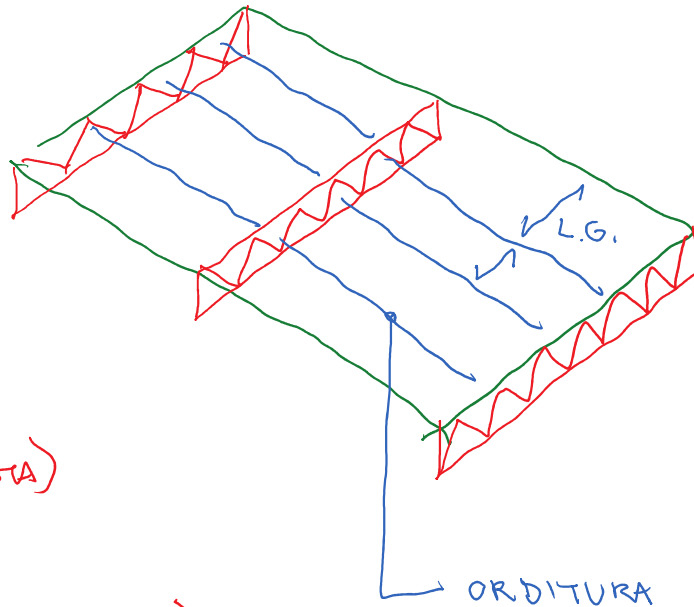
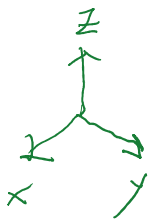


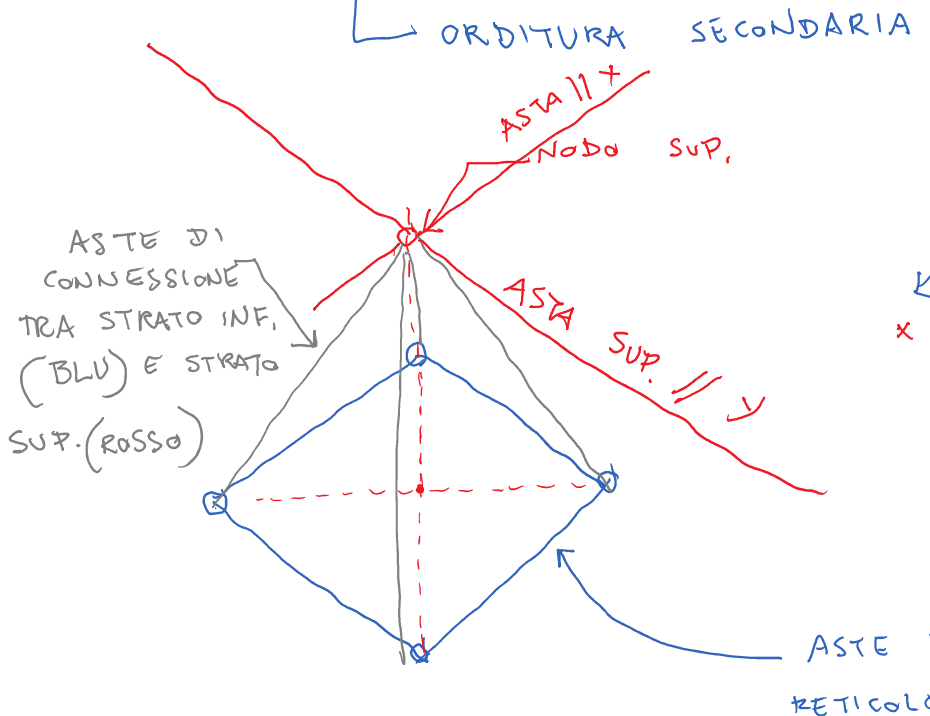
# SOLUZIONI OTTIMIZZATE PER LA STRUTTURA DI IMPALCATO

NUOVA TIPOLOGIA STRUTTURALE :  
STRUTTURA RETICOLARE SPAZIALE (3d)  
SPACE TRUSS



STRUTTURA  
RET. PIANA (CONTIGUA)  
IN UN PIANO XZ

SPACE TRUSS

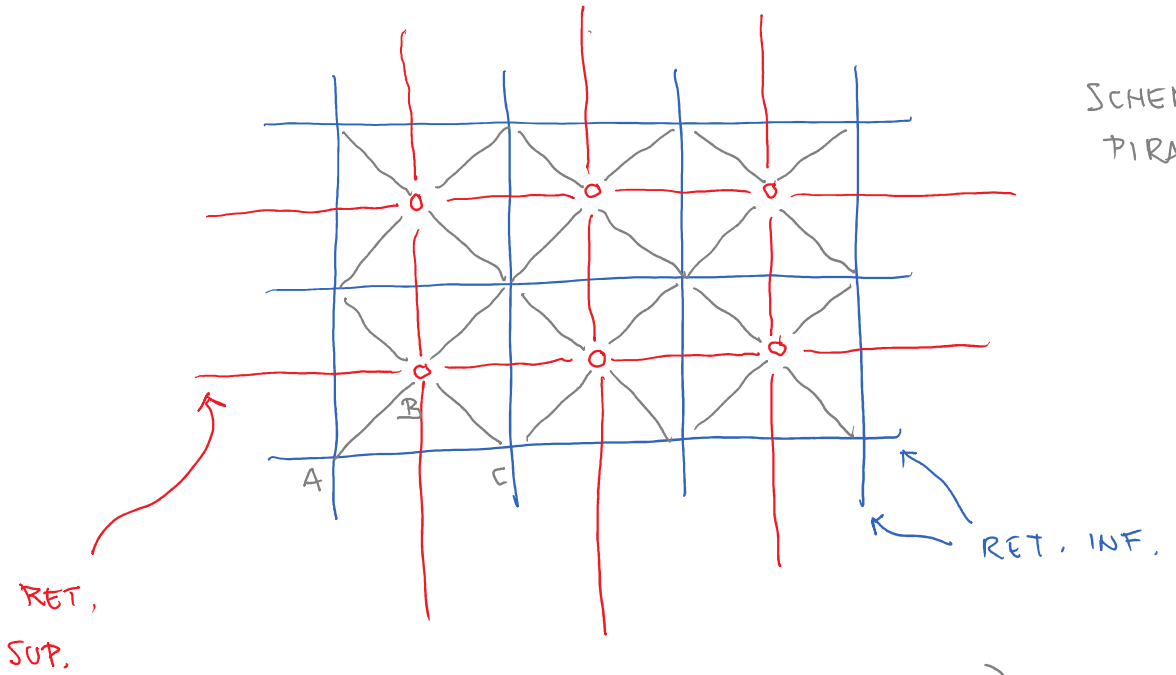


MODULO  
3d

INTERIORE

NISTA PLANIMETRICA :

SCHEMA  
PIRAMIDALE

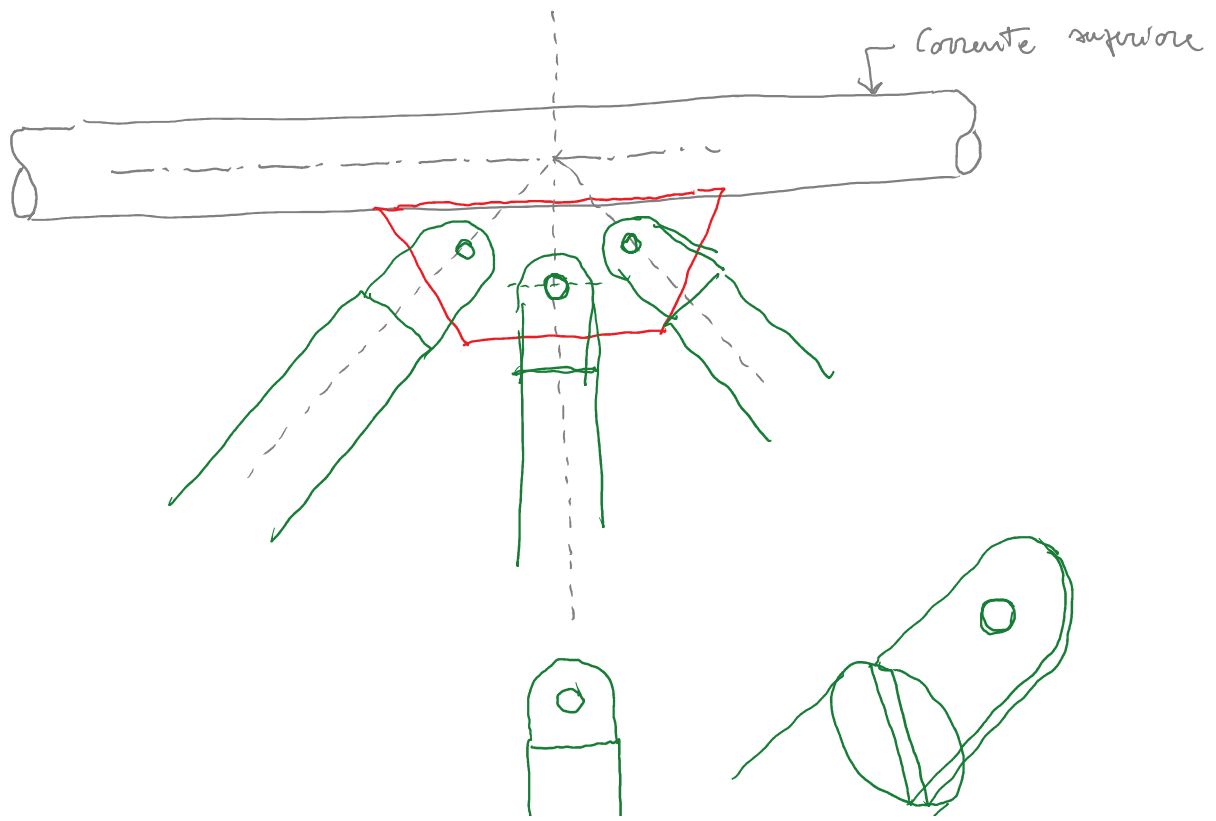


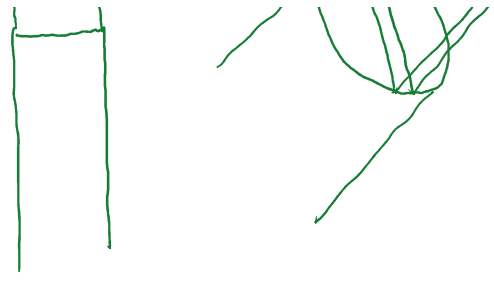
$\overline{AB} = \overline{AC}$  (SPESSE, NON SEMPRE)

aste di conn.  
stato sup. & inf.

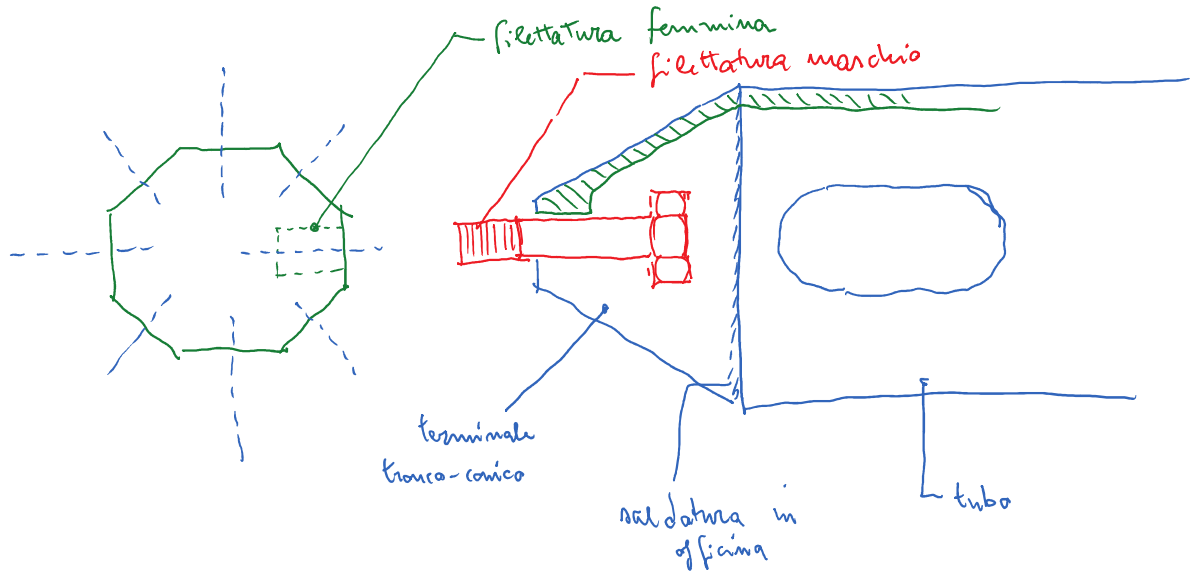
LATO DI BASE  
DELLA PIRAMIDE

NODO A FAZZOLETTO (STRUTT. RET. PIANA)



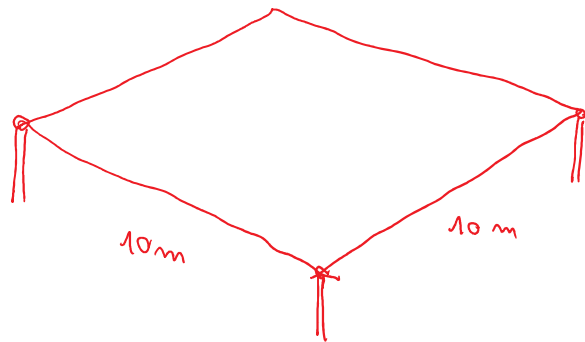


Nodo TIPO MERO



Space truss piramidale

Analisi dei carichi  
 $750 \text{ daNm}^{-2}$   
 (carichi perm. + acc. valori caratteristici)



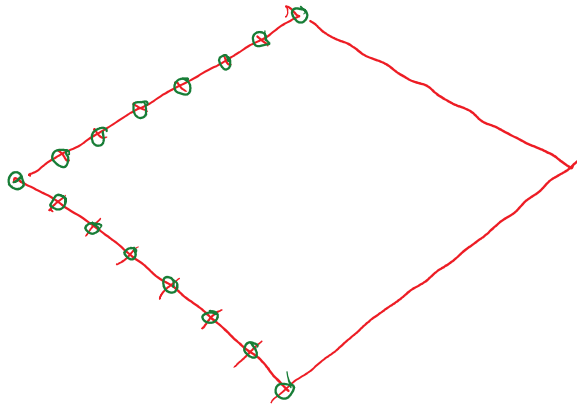
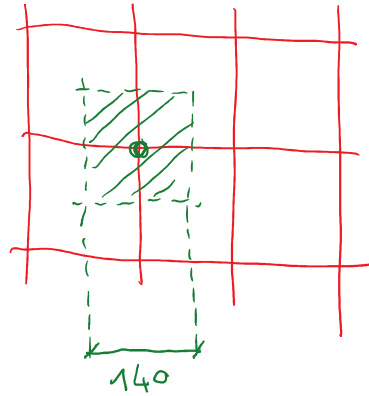
In SAP2000 :

n. of bays 1  
 lato di base 1000 cm  
 $h = 150$

mesh lato  $1000/7 \approx 143$

CARICO NODALE

$$P = 750 \text{ daNm}^{-2} \times 1.4 \text{ m}^2 = 1470 \text{ daN}$$



IN TOT. I NODI DEL PIANO RAFFIGURATO SONO 64

DEFINIAMO LA SEZIONE TIPO FSEC1  $\varnothing$  152.4/6

Max sollecitazione. 13201 daN (compressione)

Verifica di resistenza  $\sigma_{\text{MAX}} = \frac{2750 \text{ daNcm}^2}{2} = \frac{f_{yk}}{S} = 1375$

area 29.1357 cm<sup>2</sup>  
 $\sigma_{\text{MAX}} = \frac{13201}{29.13} = 453 \text{ daNcm}^{-2} \ll 1375$

Verifica di agibilit   $f \ll \frac{L}{250}$  (target)

$f_{\text{MAX}} = 0.3156$   $f = \frac{L}{K}$  si desidera  $K \geq 250$

$K = \frac{L}{f} = \frac{1000}{0.32} \approx 3000$   $f \approx \frac{L}{3000}$

Verifica di INSTABILITA' EULERIANA DELL'ASTA

Verifica di INSTABILITÀ EULERIANA DELL'ASTA COMPRESSA

$$N \leq \frac{\pi^2 E I}{L^2 S} = 218\,000 = \frac{[F]}{21}$$

$$\pi = 3.14159265$$

$$E = 2\,080\,000 \text{ daNcm}^{-2}$$

$$I = 778 \text{ cm}^4$$

$$S = \text{coeff. di sicurezza} = 2$$

$$L = 191 \text{ cm}$$

$$\frac{P_{crit}}{S}$$

$$N_{max} = 13\,200 \ll 218\,000$$

Verifica soddisfatta